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# *n*-Heptane isomerization over mesoporous $MoO_x$ and $Ni-MoO_x$ catalysts

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#### **Abstract**

 $MoO_x$  and  $Ni-MoO_x$  catalysts with maximum pore diameter at ca. 4.1 nm in the meso-pore range were prepared by reducing  $MoO_3$  or NiO doped  $MoO_3$  in  $H_2$  flow at 623 K in a period of 6-12 h. The catalysts were used in n-heptane isomerization isothermally carried out at 573 K under atmospheric pressure in a conventional fixed-bed flow reactor.  $MoO_x$  is predominantly composed of the  $MoO_xH_y$  and  $MoO_2$  phase. The former can be considered to be more active than the latter. Over the  $MoO_x$  catalyst, the  $H_2$  partial pressure positively affected the reaction rate with an order of ca. 0.35. It can be deduced from the result that the  $MoO_x$  catalyst lacks active sites with a metallic character for dehydrogenation–hydrogenation step in n-heptane isomerization. The  $Ni-MoO_x$  catalysts have a lower specific surface area than the  $MoO_x$  catalysts, due to that the reduction of  $MoO_3$  was accelerated by nickel, and the fact that more  $H_2O$  was produced in the initial reduction process, this leading to  $MoO_x$  sintering. Comparing with  $MoO_x$  catalysts, the 5%  $Ni-MoO_x$  catalysts are more active in terms of the reaction rate per unit surface area of the catalyst, the explanation is that the dehydrogenation–hydrogenation step in n-heptane isomerization is effectively enhanced by incorporation of Ni in the catalysts. © 2004 Published by Elsevier B.V.

Keywords: MoO<sub>x</sub>; Ni–MoO<sub>x</sub>; Meso-pore; Isomerization; n-Heptane

#### 1. Introduction

Environmental considerations have brought about a rapid phase out of lead additives and a braking of MTBE in gasoline in the recent years. It makes industrial isomerization processes converting linear alkanes into branched ones increasingly more important, because this processes offer a route to achieve high octane number of gasoline. Recently, molybdenum oxides (MoO<sub>x</sub>) treated in H<sub>2</sub> at 623-673 K have attracted much attention because of their high catalytic activity and selectivity for *n*-heptane isomerization. Matsuda et al. have reported that  $MoO_x$  with a maximum porosity around 0.6 nm in diameter obtained by a 12 h or longer period H<sub>2</sub> reduction of MoO<sub>3</sub> at 623 K was more active and selective for isomerization of *n*-heptane, compared with 0.5 wt.% Pt/USY zeolite. They have suggested that the  $MoO_x$  possesses bifunctional properties, which are responsible for the higher isomerization activity [1–4]. In this paper,

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we report on  $MoO_x$  and  $Ni-MoO_x$  catalysts with maximum pore volume in the meso-pore range used in the n-heptane isomerization reaction.

## 2. Experimental

### 2.1. Catalyst preparation

The MoO<sub>3</sub> used in this study was a commercial powder (Beijing Chemicals) with Analytical Purity. After being compressed into pellets, and crushed, 0.15 g of the sample (60–80 mesh) of pure MoO<sub>3</sub> or doped with nickel oxide (NiO–MoO<sub>x</sub>) was charged into a stainless steel reactor with a diameter of 3.8 mm, reduced by H<sub>2</sub> (which was purified by passing through a Pd/Al<sub>2</sub>O<sub>3</sub> catalyst and then dried with 3A molecular sieve on line). In the reduction process, the temperature was first raised from 373 to 623 K at the rate of 5 K min<sup>-1</sup> and then held at the reduction temperature for a desired period with H<sub>2</sub> flow of 120 ml min<sup>-1</sup>. To obtain the catalyst sample for characterizations, the catalyst, protected

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by  $N_2$ , was cooled to room temperature and then passivated for 3 h with a gas mixture containing 0.5%  $O_2$  in  $N_2$  to avoid bulk oxidation. The catalysts were denoted by the Ni percent in the precursors that were submitted to activation by the reduction, and the reduction period. For instance,  $MoO_3(2)$  represents the catalyst obtained by reducing  $MoO_3$  in  $H_2$  for 2 h, and 5% Ni $-MoO_3(6)$  denotes that the catalyst obtained from a NiO $-MoO_3$  precursor with Ni/(Ni + Mo) molar ratio 5%, reduced in  $H_2$  for 6 h.

#### 2.2. Catalyst characterization

Crystalline phases of the catalysts were characterized in Riguka D/max 2400 X-ray diffractometer using Cu K $\alpha$  radiation under 40 kV and 100 mA. To evaluate the percentage of MoO<sub>3</sub> retained in the MoO<sub>3</sub>(2) catalyst, a set of mechanically mixed samples containing different amounts of MoO<sub>3</sub> and MoO<sub>3</sub>(12) were determined by XRD in uniform analyzing conditions. BET surface area and pore size distribution of the catalysts were determined at liquid nitrogen temperature by a Micrometritics ASAP-2000 adsorption analyzer.

### 2.3. Catalytic activity measurement

The isomerization of n-heptane was isothermally carried out at 573 K under atmospheric pressure in a conventional fixed-bed flow reactor. The catalyst being submitted to the activity measurement was prepared in situ without undergoing passivation. The reactant gas containing n-heptane,  $H_2$ , and  $N_2$  (as complement gas) was fed in the reactor downwards with a total flow rate 125.3 ml min $^{-1}$ . The composition of effluent gas was analyzed by means of FID gas chromatography using quartz capillary separation column. The selectivity to iso- $C_7$  was defined as the ratio of iso- $C_7$  products to n- $C_7$  transformed in terms of moles.

## 3. Results and discussion

# 3.1. The $MoO_x$ catalysts

The physico-chemical structure of  $MoO_x$  catalysts obtained by reducing  $MoO_3$  in  $H_2$  at 623 K for different period were characterized in their bulk and surface properties. As shown in Fig. 1, almost all  $MoO_3$  in sample  $MoO_3(2)$  is reduced by hydrogen, though the diffraction lines  $(2\theta = 12.7^\circ, 25.42^\circ, 38.48^\circ)$  corresponding to  $MoO_3$  phases are still detected. It was determined quantitatively by the XRD method that less than 1/30 of molybdenum maintained the original  $MoO_3$  phase in the  $MoO_3(2)$  sample. In the  $MoO_3(6)$  sample, the diffraction lines of  $MoO_3$  phases completely disappear. The sample consists of  $MoO_2$  and some phases with diffraction lines at  $2\theta = 14.4^\circ$  (d = 0.6137 nm),  $2\theta = 29.3^\circ$  (d = 0.3048 nm),  $2\theta = 38.3^\circ$  (d = 0.2346 nm), and  $2\theta = 44.4^\circ$  (d = 0.2037 nm). This indicates that  $MoO_3$  can be easily reduced by  $H_2$  at 623 K in our reduction condi-

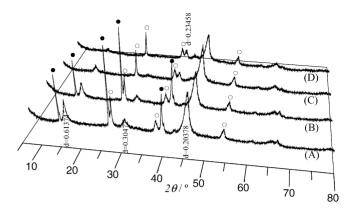


Fig. 1. XRD patterns of  $MoO_x$  obtained by reducing  $MoO_3$  in  $H_2$  at 623 K for different periods: (A) 2 h; (C) 6 h; (D) 12 h; (B) 1 h (which was then submitted to *n*-heptane isomerization reaction for 1 h). ( $\blacksquare$ ) Peaks corresponding to  $MoO_3$ ; ( $\bigcirc$ )  $MoO_2$ .

tions. In the XRD diagrams, it seems that the diffraction lines at  $2\theta = 14.4^{\circ}$  and  $29.3^{\circ}$  diminish simultaneously when the reduction period is prolonged. Taking account of that the d-value 0.6137 nm of the former is almost equal to the double of that of the latter, it is suggested that both diffractions belong to the same crystalline phase H<sub>x</sub>MoO<sub>3</sub>. On the other hand, the two diffraction lines at 38.3° and 44.4°, being hardly changed in intensity when the reduction period increases, can be considered to be derived from a MoO<sub>x</sub>H<sub>y</sub> phase. Leclercq and co-workers reported that  $MoO_xC_y$  prepared by the decomposition of Mo(CO)<sub>6</sub> gave diffraction lines at  $2\theta = 38^{\circ}$  and  $44^{\circ}$  [5,6]. Delporte et al. [7] stated that a treatment of MoO3 with a mixture of H2 and hydrocarbon at 623 K yielded the  $MoO_xC_y$  phase, and that hydrogen was able to act like carbon atoms to form  $MoO_xH_y$ , of which the diffraction line appeared at  $2\theta = 44.3^{\circ}$ . Matsuda et al. also suggested that the two peaks at  $2\theta = 38.1^{\circ}$  and  $44.3^{\circ}$  were associated with the formation of the MoO<sub>x</sub>H<sub>y</sub> phase. Although the diffraction lines at d = 0.6137 nm ( $2\theta$  $= 14.4^{\circ}$ ),  $d = 0.3048 \,\mathrm{nm} \,(2\theta = 29.3^{\circ})$  and  $d = 0.2037 \,\mathrm{nm}$  $(2\theta = 44.4^{\circ})$  in Fig. 1 are very close to those d = 0.6198, 0.3057, and 0.2038 nm of the  $Mo_xO_yC_z$  phase reported by Ledoux et al. [8], the presence of a carbon-containing phase can be excluded here, since the reduction process was carefully controlled to be free of hydrocarbons in our experiments. In favor of this conclusion is the fact that the catalyst sample MoO<sub>3</sub>(1) which was obtained by one hour's hydrogen-reduction of MoO<sub>3</sub> at 623 K and then submitted to *n*-heptane isomerization for 1 h at the same temperature, did not show a stronger intensity of the three peaks than those of  $MoO_x$  sample as-prepared by pure  $H_2$  reduction, as shown in Fig. 1. This shows that carbon is not incorporated in the sample even in more favorable conditions.

From Fig. 1, it can be also observed that the relative intensity of the diffractions due to the  $MoO_xH_y$  and  $MoO_2$  phases are almost unchanged irrespective of the reduction period, indicating that both phases in the  $MoO_x$  catalysts were formed simultaneously in the reduction process of

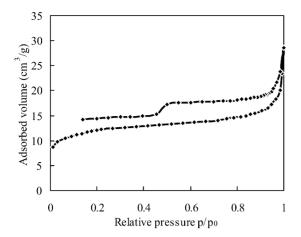


Fig. 2. Adsorption-desorption isotherms of N<sub>2</sub> on MoO<sub>3</sub>(12h).

MoO<sub>3</sub>. Compared with the XRD patterns that presented by Matsuda et al. in literature [2,9], MoO<sub>x</sub>(12h) shows a stronger diffraction intensity of those due to MoO<sub>x</sub>H<sub>y</sub> and a weaker intensity of MoO<sub>2</sub>, indicating that the MoO<sub>x</sub>(12h) catalyst contains more MoO<sub>x</sub>H<sub>y</sub> phases and less MoO<sub>2</sub> phases than that reported by the authors [1,2,9].

The physical structure of the  $MoO_x$  catalysts in our study markedly differs from that mentioned in literature data, in which some  $MoO_x$  samples with surface area of  $170-180 \,\mathrm{m^2\,g^{-1}}$  and with a maximum pores volume at diameter of ca.  $0.6 \,\mathrm{nm}$  were reported [2,9]. Concerning all the  $MoO_x$  catalysts we tested, the BET equation provided satisfactory linear fit of the  $N_2$  adsorption data. This gave BET surface areas of 36.2 and  $41.6 \,\mathrm{m^2\,g^{-1}}$  for  $MoO_3(6)$  and  $MoO_3(12)$ , respectively. The  $MoO_x$  catalysts exhibited obvious  $N_2$  adsorption—desorption hysteresis in the relative pressure,  $p/p_0$ , in the range of ca. 0.5-0.9985. The hysteresis on  $MoO_3(12)$  is displayed in Fig. 2. The corresponding pore-size distribution curve (Fig. 3) being calculated on the basis of the  $N_2$  desorption data shows a maximum pore volume diameter at ca.  $4.1 \,\mathrm{nm}$  in meso-pore range.

In recent years, the surface area of MoO<sub>3</sub> has been extensively reported to be enlarged after a temperature-programmed reaction with NH<sub>3</sub> [10–13], carburization under H<sub>2</sub> and hydrocarbon mixtures [7,14,15], and in H<sub>2</sub> reduction [7].

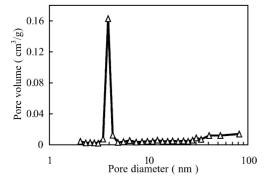


Fig. 3. Pore-size distribution for MoO<sub>3</sub>(12 h).

The following mechanism has been proposed to explain the results: The reduction of  $MoO_3$  begins preferentially at the crystallographic defects, and as the reduction proceeds, the contraction of lattice fractures the crystal wherein [16]. According to this mechanism, the measured meso-pores characterized by the  $N_2$  adsorption—desorption hysteresis can be considered as reflecting the clearance between some uniform nano-particles of  $MoO_x$  being formed as a consequence of crystal rupture. This suggestion may also be supported by the fact that the  $MoO_x$  samples do not present small angle X-ray scattering (SAXS) being characteristic of regular meso-pore structure similar to that of meso-pore molecule sieves, as shown in Fig. 1.

The activity of the  $MoO_x$  catalysts for *n*-heptane isomerization at 573 K strongly depends on the reduction period. As shown in Fig. 4, n-heptane conversion sharply increased with the reduction period of the catalyst in the first hours and then reached a constant value when the reduction period was prolonged to 12 h. The changes in catalyst activity versus the reduction period are quite consistent with the considerable modification in the bulk composition of MoO<sub>x</sub> illustrated in Fig. 1, observed within the reduction period of 12h, especially in the first 6h. The  $MoO_x(12h)$  catalyst gave 50.3% conversion of *n*-heptane in the following conditions:  $W/F = 11.0 \,\mathrm{g_{cat}} \,\mathrm{h} \,\mathrm{mol} \,\mathrm{C_7}^{-1}$ , and  $\mathrm{H_2}/n$ -heptane = 23 (in volume ratio). In Ref. [1], an *n*-heptane conversion of 46.1% in the conditions of  $12.5 \, g_{cat} \, h \, mol \, C_7^{-1}$  of W/F, 40 of H<sub>2</sub>/n-heptane ratio in volume, at 573 K was achieved over a  $MoO_x(24 \text{ h})$  catalyst with a specific surface area 47.9 m<sup>2</sup> g<sup>-1</sup> obtained by 24 hours' hydrogen reduction of MoO<sub>3</sub>. Taking the differences of reaction conditions into account, it seems that the  $MoO_x(12 h)$  catalyst with a specific surface area  $41.6 \,\mathrm{m}^2 \,\mathrm{g}^{-1}$  being composed of more  $\mathrm{MoO}_x \mathrm{H}_v$ phases and less MoO2 phases has higher activity in unit surface for the *n*-heptane isomerization, in comparison with the  $MoO_x(24 h)$  catalyst mentioned in literature [1]. From these results, it can be deduced that the MoO<sub>x</sub>H<sub>y</sub> phase is more

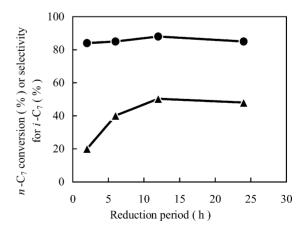


Fig. 4. The catalytic activity of  $\text{MoO}_x$  for *n*-heptane isomerization prepared in different reduction period at 623 K (( $\triangle$ ) *n*-C<sub>7</sub> conversion; ( $\bigcirc$ ) selectivity for *i*-C<sub>7</sub>). Reaction conditions: T = 573 K,  $\text{H}_2/n\text{-C}_7 = 25$ ;  $W/F = 11 \text{ g}_{\text{cat}} \text{ h} \text{ mol}^{-1}$ .

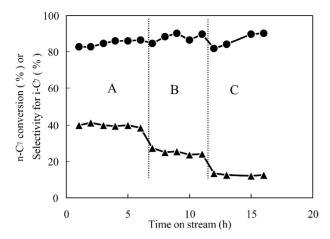


Fig. 5. The dependence of *n*-heptane conversion on partial pressure of  $H_2$ : ( $\blacktriangle$ ) n- $C_7$  conversion; ( $\blacksquare$ ) selectivity for i- $C_7$ . (A)  $p_{\rm H_2} = 97.0\,{\rm kPa}$ , (B)  $p_{\rm H_2} = 48.5\,{\rm kPa}$ , (C)  $p_{\rm H_2} = 24.2\,{\rm kPa}$ . Reaction conditions:  $T = 573\,{\rm K}$ ,  $W/F = 11\,{\rm g_{cat}}\,{\rm h}\,{\rm mol}^{-1}$ , total flow rate  $= 125.3\,{\rm ml}\,{\rm min}^{-1}$ .

active for n-heptane isomerization than the MoO<sub>2</sub> phase. In some previous investigations [17,18], this has to be noticed, it seems that the role of the MoO<sub>2</sub> phase in alkane isomerization has been strongly emphasized by the researchers.

Taking notice of the difference with respect to the  $H_2/n$ -heptane ratio used in n-heptane isomerization between that in our research and that in the literature, the influence of  $H_2$  partial pressure on the reaction was investigated. The effect of  $H_2$  partial pressure is illustrated in Fig. 5. In reaction conditions where we kept constant the n-heptane feed, and the total flow rate of the reactant gas mixture (including complementary gas of  $N_2$ ) to be  $125.3 \,\mathrm{ml}\,\mathrm{min}^{-1}$ , the n-heptane conversion over  $\mathrm{MoO}_x(6\,\mathrm{h})$  catalyst exhibits a sharp decline with the decrease of the  $H_2$  partial pressure, indicating that the  $H_2$  partial pressure exerts a positive contribution to n-heptane isomerization. This implies that the conversion of n-heptane would be much higher than 50.3%, over the  $\mathrm{MoO}_x(6\,\mathrm{h})$  catalyst if the reaction proceeded at the  $H_2/n$ -heptane ratio of 40 that was used in literature [1].

From Fig. 5, a reaction order of 0.35 with respect to  $H_2$  partial pressure in the n-heptane isomerization over the  $MoO_3(6 \text{ h})$  catalyst was obtained, by plotting  $\ln(FC)$  versus  $\ln p_{H_2}$ , where F, C and  $p_{H_2}$  denote the flow rate of n-heptane, its conversion, and partial pressure of  $H_2$ , respectively. It differs from the Pd/SAPO-11 catalyst [19] and the oxygen-modified molybdenum carbide catalyst [20], over which negative reaction orders for  $H_2$  partial pressure were obtained. Comparing to classical bifunctional catalysts, the  $MoO_x$  catalyst seems to possess more acidic sites active for isomerization step and less active sites with a metallic character for the dehydrogenation—hydrogenation step, if we take into account the bifunctional properties of  $MoO_x$  [1].

# 3.2. The 5% Ni– $MoO_x$ catalysts

Nickel is well known as an effective component of catalyst in reaction involving H<sub>2</sub> activation. To improve the metal-

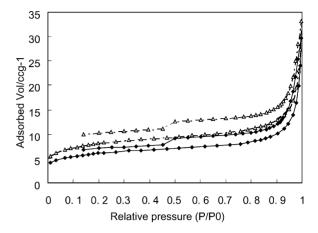


Fig. 6. The adsorption–desorption isotherms of  $N_2$  on Ni–MoO<sub>3</sub> catalysts:  $(\spadesuit)$  Ni–MoO<sub>3</sub>(6 h)  $(\triangle)$  Ni–MoO<sub>3</sub>(12 h).

lic function of  $MoO_x$  in the *n*-heptane isomerization, nickel doped  $MoO_x$  catalysts were investigated. The 5% Ni– $MoO_x$  catalysts give also satisfactory linear BET relation and evident hysteresis with respect to the  $N_2$  relative pressure, as shown in Fig. 6. Although the 5% Ni– $MoO_x$  catalysts had been prepared by hydrogen reduction in the same way as that of the  $MoO_x$  catalysts, they unfortunately exhibited a specific BET surface area of only 21.4 and 28.6 m<sup>2</sup> g<sup>-1</sup> for the 5% Ni– $MoO_x$ (6 h) and 5% Ni– $MoO_x$ (12 h), respectively, which is obviously less than that of the counterpart of the  $MoO_x$  catalysts. On the other hand, the 5% Ni– $MoO_x$  catalysts have the same maximum pore diameter ca. 4.1 nm as that of the  $MoO_x$  catalysts, as shown in Fig. 7.

The chemical bulk properties of the 5% Ni–MoO<sub>x</sub> catalysts are reported in Fig. 8. Comparing with  $MoO_x$  catalysts, the 5% Ni–MoO $_x$  catalysts seems to have less MoO $_2$ phases (corresponding to the diffractions at  $2\theta = 26.1^{\circ}$ ,  $37.0^{\circ}$ ,  $53.6^{\circ}$ ), in comparison to the MoO<sub>x</sub>H<sub>y</sub> phases. Tt can also be observed that the nickel oxide doped MoO<sub>3</sub> was more easily reduced by H<sub>2</sub> than pure MoO<sub>3</sub> at 623 K. Whereas the sample still contained about 1/30 of MoO<sub>3</sub> when it was reduced for 2 h in the case of  $MoO_x(2 h)$ , no  $MoO_3$  phase was detectable in the case of 5% Ni–MoO<sub>x</sub>(2h). The promotion due to the nickel component for the MoO3 reduction may be attributed to its effective function for H<sub>2</sub> activation. The promotion may also concern the *n*-heptane isomerization results. For example, the catalyst prepared by hydrogen reduction of MoO<sub>3</sub> for 12 h at 573 K, provided only 7.5% of the *n*-heptane conversion, while on the catalyst prepared from nickel oxide (5 wt.%) doped MoO<sub>3</sub> in the same reduction conditions, 27.5% of *n*-heptane conversion was achieved.

It was reported that  $Mo_2N$  with larger surface area was synthesized in temperature-programmed reaction of  $MoO_3$  and  $NH_3$ . The resultant high surface area was achieved only when the reaction took place at a slow, controlled rate and in a greater space velocity of  $NH_3$  [16,21]. The reason suggested by the authors was that, the presence of  $H_2O$  vapor produced by the reduction might cause sintering of the prod-

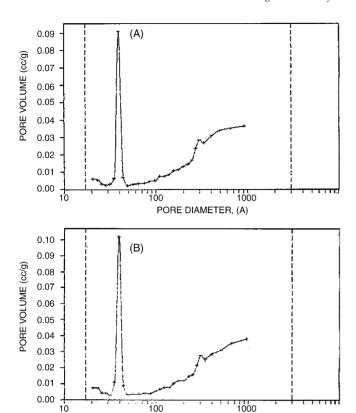


Fig. 7. Pore-size distributions for Ni–MoO<sub>x</sub> catalysts: (A) Ni–MoO<sub>x</sub>(6 h), (B) Ni–MoO<sub>x</sub>(12 h).

PORE DIAMETER, (A)

uct  $Mo_2N$ . The favorable effect was supposed to be due to the fact that the partial pressure was lowered in the conditions of slow reduction rate and large flow rate of the reactive gas [16]. Recently, Matsuda et al. in some experiments further confirmed the suggestion. They found that the surface area of  $MoO_x$  was strongly influenced by the partial pressure of  $H_2O$  mixed with the reactive gas  $H_2$  [9]. In the case of  $Ni-MoO_x$  catalysts, the reduction of  $MoO_3$  is accelerated by the nickel component, and the increased production of  $H_2O$  in the initial reduction steps leads to  $MoO_x$  sintering, so that  $Ni-MoO_x$  sample with less surface area than that of  $MoO_x$  is obtained.



Catalyst	BET surface (m <sup>2</sup> /g)	Conversion of <i>n</i> -C <sub>7</sub> (%)	Relative activity on unit surface area <sup>b</sup>	Selectivity to <i>n</i> -C <sub>7</sub> (%)
$MoO_x(2 h)$	_a	20.0	_a	84
$MoO_x(6h)$	36.1	40.1	1	85
$MoO_x(12 h)$	41.6	50.3	1.1	88
5% Ni–MoO $_x(2 h)$	_a	30.9	_a	87
5% Ni–MoO $_x$ (6h)	21.4	43.6	1.8	86
5% Ni–MoO $_{x}(12 \text{ h})$	28.6	45.3	1.4	80
5% Ni + MoO <sub>x</sub> (6 h)	_a	51.8	1.3°	82

<sup>&</sup>lt;sup>a</sup> Not measured, or calculated.

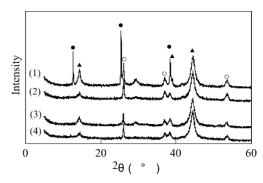


Fig. 8. XRD patterns of  $MoO_x$  and  $Ni-MoO_x$  catalysts reduced in different periods (1)  $MoO_x$  reduced for 2 h, (2) for 6 h, (3)  $Ni-MoO_x$  reduced for 2 h, (4) for 6 h, corresponding to  $MoO_3$  ( $\blacksquare$ ),  $MoO_2$  ( $\bigcirc$ ),  $MoO_xH_y$  ( $\blacktriangle$ ).

The catalytic performance of the 5% Ni–MoO<sub>x</sub> catalysts in n-heptane isomerization is summarized in Table 1. The 5% Ni-MoO<sub>x</sub> catalysts are not superior to the counterpart  $MoO_x$  catalysts when activity in per gram in *n*-heptane isomerization is considered, due to their lower specific surface areas. However, in terms of reaction rate per unit surface area, all the 5% Ni-MoO<sub>x</sub> catalysts have a higher activity than the  $MoO_x$  catalysts in the same reaction conditions. Nevertheless, from the view point of catalysis, it remains still not clear whether the nickel component is favorable for *n*-heptane isomerization or not. The reason is that the 5%  $Ni-MoO_x$  and  $MoO_x$  catalysts contain different percentages of MoO<sub>x</sub>H<sub>y</sub> phase. To further evaluate the effect of nickel component in the catalytic *n*-heptane isomerization, 0.133 g of a mechanical mixture, composed of  $0.13 \,\mathrm{g}$  of  $\mathrm{MoO}_{x}(6 \,\mathrm{h})$ (which corresponds to 0.15 g of MoO<sub>3</sub>, assuming that all of molybdenum in  $MoO_x$  exists as  $MoO_2$ ) and 0.003 g of nickel metal powder, had been pressed into 60-80 mesh, and was tested as catalyst in the same reaction conditions. As shown in Table 1, the mixture provides 51.8% of *n*-heptane conversion, after being pretreated in H<sub>2</sub> at 573 K for half an hour. This indicates that, in the case of 5% Ni-MoO<sub>x</sub>, the addition of NiO to MoO<sub>3</sub> is not only in favor of the MoO<sub>2</sub>H<sub>y</sub> phases formation in the reduction process, but also facilitates n-heptane isomerization, by activating  $H_2$  and therefore enhancing the dehydrogenation-hydrogenation step in

<sup>&</sup>lt;sup>b</sup> Relative to that of  $MoO_x(6h)$  which defined activity unit.

<sup>&</sup>lt;sup>c</sup> Calculated by assuming that the Ni powder does not provide surface area and that all molybdenum in MoO<sub>x</sub> existed as MoO<sub>2</sub>.

n-heptane isomerization over  $MoO_x$ . Of course, the diminution of the catalyst surface area and decrease of selectivity to n-heptane isomerization in the reaction owing to the addition of nickel are not satisfactory. These disadvantages might probably overcome by activating the catalyst at lower reduction temperature and using it at lower reaction temperature, respectively.

#### 4. Conclusion

 $MoO_x$  catalysts with maximum pore volume diameter at ca. 4.1 nm in meso-pore range can be obtained by reducing  $MoO_3$  in  $H_2$  flow at 623 K over a period of 6–12 h. The meso-pores characterized by the  $N_2$  adsorption–desorption hysteresis can be considered as reflecting the clearance between uniform nano-particles of  $MoO_x$  being formed as a consequence of the crystal rupture of  $MoO_3$ .

The  $MoO_x$  is predominantly composed of  $MoO_xH_y$  phase and  $MoO_2$  phase, and the former phase can be considered to be more active than the latter one for n-heptane isomerization. Over the  $MoO_x$  catalyst, the  $H_2$  partial pressure positively affects the reaction rate with an order of ca. 0.35, therefore it can be deduced from the result that the  $MoO_x$  catalyst lacks active sites for dehydrogenation—hydrogenation step in n-heptane isomerization.

By incorporation of NiO into MoO<sub>3</sub>, Ni–MoO<sub>x</sub> catalysts with maximum pore volume diameter at ca. 4.1 nm can be obtained in the same way as for the MoO<sub>x</sub> catalysts. The Ni–MoO<sub>x</sub> catalysts thus obtained have a specific surface area lower than the MoO<sub>x</sub> catalysts, because the reduction of MoO<sub>x</sub> is accelerated by the nickel component, and more H<sub>2</sub>O is produced in the initial reduction process, this leading to MoO<sub>x</sub> sintering. Comparing with MoO<sub>x</sub> catalysts, the 5% Ni–MoO<sub>x</sub> catalysts are more active in terms of the reaction rate per unit surface area of the catalyst. The explanation is that the dehydrogenation–hydrogenation step in n-heptane

isomerization is effectively enhanced by the incorporation of Ni in the catalysts.

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